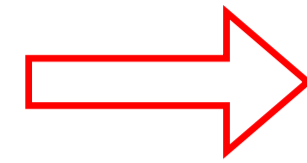


Study of development of atmospheric boundary layer under various atmospheric stability

大気汚染拡散の予測

大気境界層の拡散性状は、大気安定度によって強い影響を受けるため

大気境界層の拡散性状の把握が不可欠



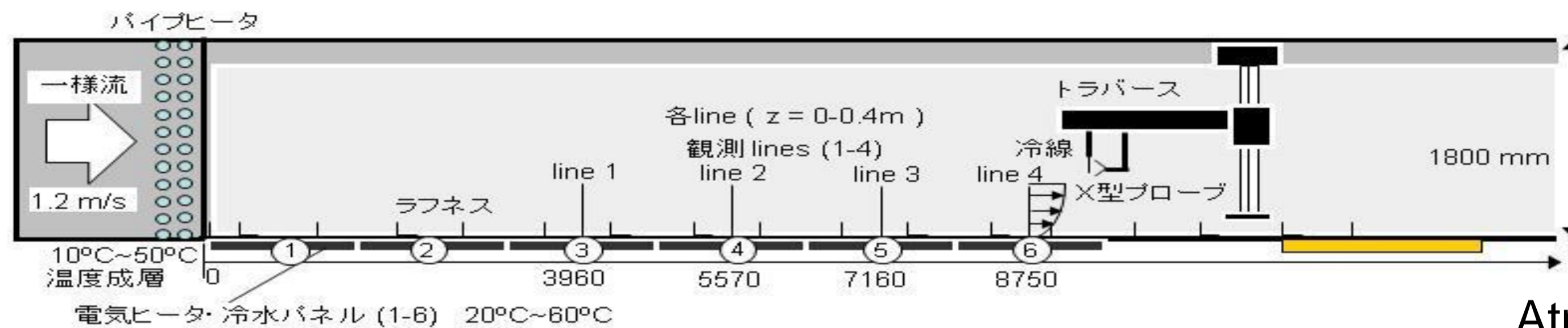
CFDと風洞実験の併用による

様々な大気安定度条件下での大気境界層の発達過程を検討



数值的に安定かつ簡便で様々な大気安定度条件下で利用可能なk-εモデルの提案

Outline of experiment



X型熱線風速計
I型冷線温度計による
同時計測(計測時間120秒)
(サンプリング周波数1kHz)

Wind tunnel

Atmospheric stability

測定時間 : 120秒
鉛直方向測定点数:
床上 5mm, 10mm~400mm
(間隔 10mmごと) 合計41点

| Case | Air flow temperature | Ground temperature | Ground temperature | Bulk Richardson number |
|------------------------|----------------------|--------------------|--------------------|------------------------|
| Case 1 (Neutral) | 20 °C | 20 °C | 1.22 m/s | 0 |
| Case 2 (Strong stable) | 48 °C | 20 °C | 1.20 m/s | 0.23 |
| Case 3 (Weak stable) | 33 °C | 20 °C | 1.20 m/s | 0.12 |
| Case 4 (Unstable) | 12 °C | 60 °C | 1.18 m/s | -0.47 |

$$\text{Bulk Richardson number} = gZ_{400}(T_{400} - T_S) / ((T + 273.15)(U_{400})^2)$$

Outline of CFD analysis

| | | | |
|-----------------------------|--|--------------------------------|--|
| Turbulence model | Standard k-ε model, Proposed k-ε model | | |
| Momentum transport equation | First order upwind scheme | Convection term | |
| | Second order central difference scheme | Other terms | |
| Analysis domain | 16.47 m (x), 1.8 m (y) and 1.8 m (z) | | |
| Number of mesh | 120 (x) × 40 (y) × 60 (z) | | |
| Size of mesh | 0.01 m (Near the ground) | | |
| Boundary condition | Momentum | Turbulent kinetic energy | Temperature |
| Top | u, v free slip w = 0 | Free slip | Adiabatic |
| Side | u, w free slip v = 0 | Free slip | Adiabatic |
| Inlet | Uniform flow | Turbulent intensity: 3 % | Constant temperature |
| | | Turbulent length scale: 0.36 m | |
| Outlet | Free slip | | Free slip |
| Ground | Z ₀ logarithmic law Roughness height | Free slip | Z ₀ logarithmic law Roughness height |
| | (3.0 × 10 ⁻⁴ m) | | (4.1 × 10 ⁻⁵ m) |
| Analysis algorithm | SIMPLE | | |

Proposed k-ε model

従来のk-εモデルの延長上に比較的簡易で安定かつ精度の高い大気安定度を考慮した新しいモデルの開発をめざす。

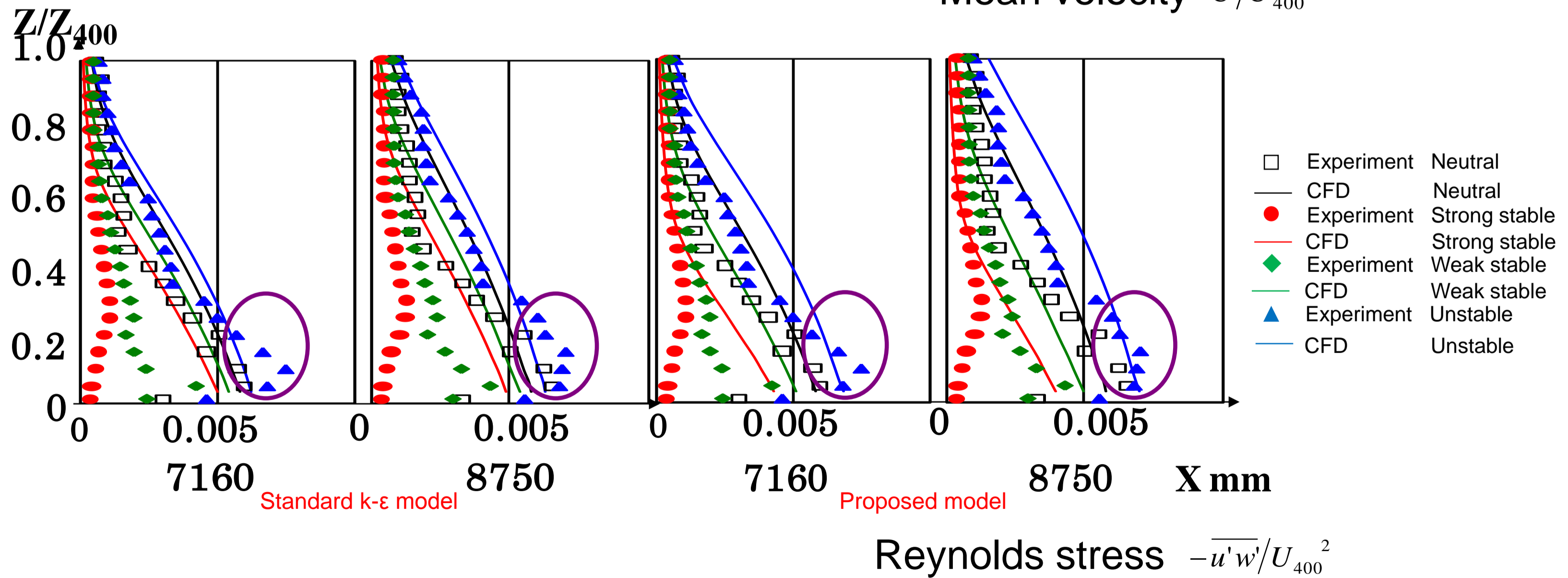
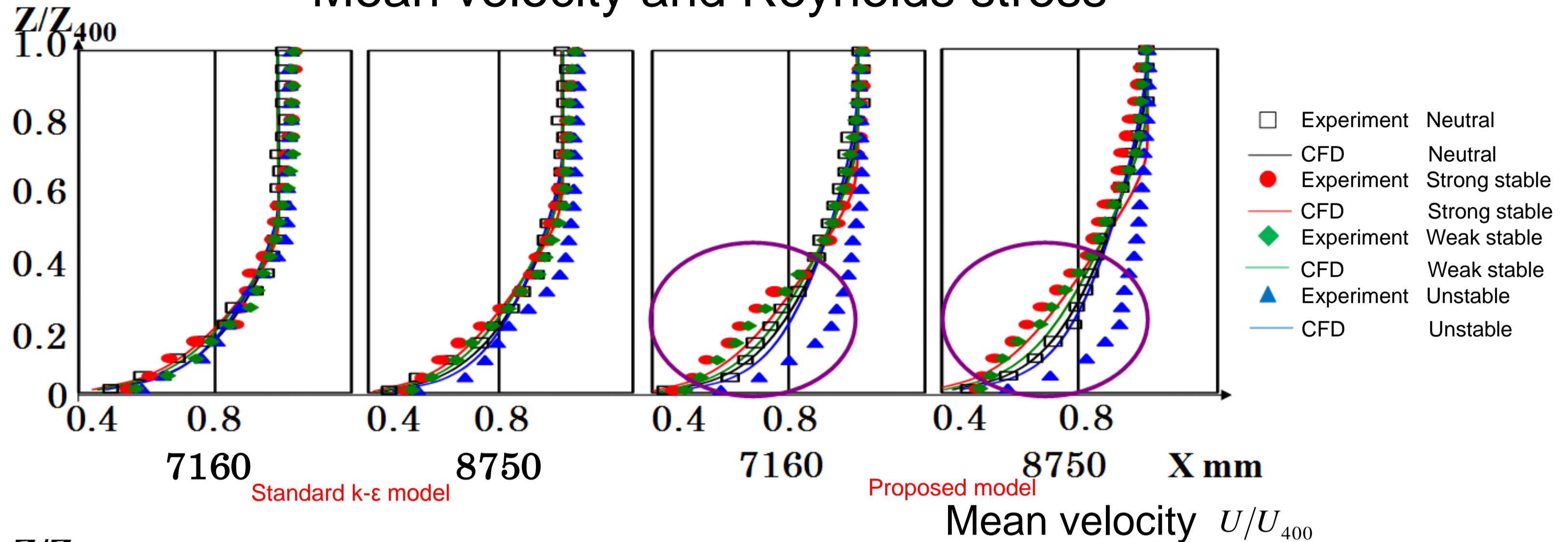
WETモデルのコンセプトに基づき、レイノルズストレスの表現は以下のようにモデル化した。

$$\overline{u_i u_j} = -(1 + G_k / P_k) \nu_t \left(\partial U_i / \partial X_j + \partial U_j / \partial X_i \right) + 2/3 k \delta_{ij}$$

但し、数値不安定を避けるために、暫定的に $0.1 < (1.0 + G_k / P_k) < 6.0$ の制約

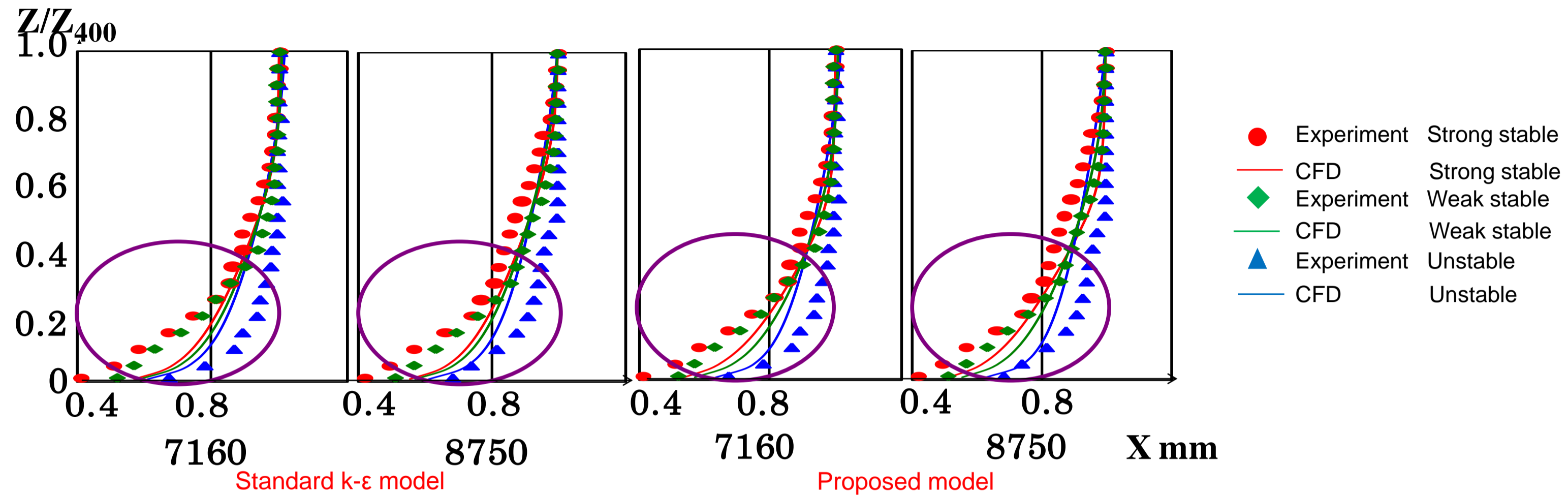
Comparison between standard k-ε model and proposed model

Mean velocity and Reynolds stress

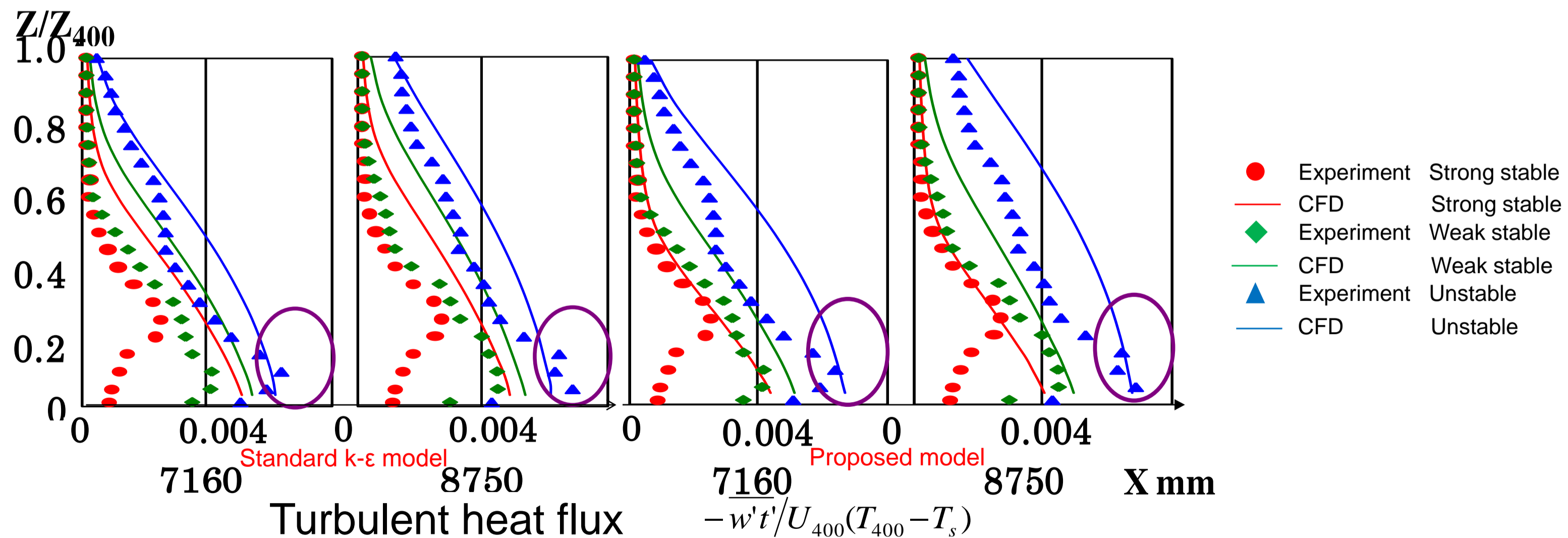


Comparison between standard k-ε model and proposed model

Mean temperature and turbulent heat flux



Mean temperature $(T - T_s)/(T_{400} - T_s)$



Turbulent heat flux $-w't'/U_{400}(T_{400} - T_s)$